Simply faster – Systematic handling

Systems | Actuators | Modules

Application description

Safe limited speed





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As at: 2019-06-07

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2 Introduction

Note: The machine manufacturer must check in advance that the required PL of the application is achieved with this module.

Please note that the speeds for each application must be calculated individually by the customer taking into account the reaction times.

Under certain circumstances, it may be necessary to use a deadman's switch or even a two-hand release.

The sample program provided is not a finished program suitable for every application. The programming, safety inspection and acceptance of the machine must be carried out by the customer. Afag Hardt GmbH assumes no liability that the components used here will achieve the required PL.

This application description shows how an eps EDP linear motor handling system can be operated at a safely reduced speed.

For each axis to be controlled, a servo controller with an STO input, an external path measuring system and a safety module are required.

In the example application, two speeds are defined for set-up operation. Reduced speed 1 is designed to work directly on the handling and reduced speed 2 is for observation with the safety door open.

The values for the safely reduced speeds were defined here for the Y-axis and Z-axis in the same way.

Reduced speed 2 may only be driven with an additional dead man's switch.

If the safety door is closed, the handling can move at maximum speed.

Safe limited speed 1 1 m/min 0.017 m/s Safe limited speed 2 2 m/min 0.03 m/s

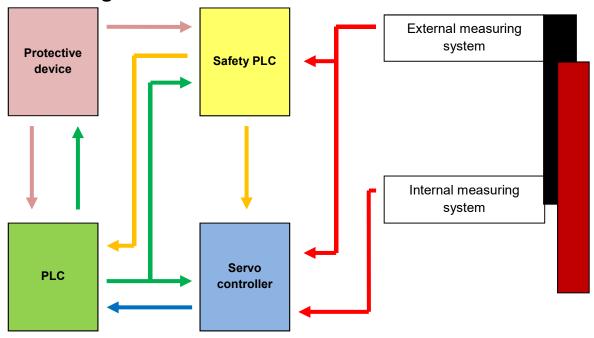
These speeds were determined for this test application on the basis of empirical values.

3 Explanation of terms

SLS	Safe Limited Speed	Sicher reduzierte Geschwindigkeit
STO	Safe Torque Off	Sichere Drehmomentabschaltung



4 Block diagram



5 How it works

To guarantee that speed is safely limited for setup mode, an additional safety module and additional external measuring system are used.

This safety module monitors the speed of handling with the help of the additional measuring system. If the previously defined maximum set-up speed is exceeded, the safety electronics switches off the release of the controller by means of safe contacts and the STO is triggered at the controller. The safety module monitors all signal channels of the measuring system and compares it with two processors for plausibility.

In addition to the monitoring by the safety module, the controller also compares the values of the internal and external measuring system. If a difference in position is detected, e.g. due to a cable break, the controller disconnects the load circuit via safety contactors.

The safety module also provides standstill monitoring. This can be utilized in various ways, e.g. to release the safety door lock.



Components used

6.1 Safeline safety PLC with

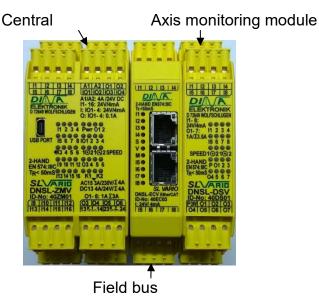
- Central module DNSL-ZMV 40ZM01
- Field bus module, e.g.

EtherCAT DNSL-ECV 40EC03 **Profibus** DNSL-DPV 40DP04 **Profinet** DNSL-PNV 40PN03 CANopen DNSL-COV 40CO03

Drive monitoring module DNSL-DSV 2 40DS01 (for 2 axes)

Note:

Up to 13 drive monitoring modules (for 26 axes) can be mounted in series



6.2 Servo controller C1xx0-xx-XC-1S





6.3 Linear path measuring system (for linear axes)

- Magnetic sensor MSK500 with filter ftaps4 (TTL 5 V)
- Magnetic tape MB500

Alternatively

- Magnetic sensor MSA501 (TTL 5 V)
- Magnetic tape MBA501
- Magnetic sensor MSK1000 with filter ftaps4 (TTL 5 V)
- Magnetic tape MB100



6.4 Encoder (for SE20)

• IE3 L with 128 pulses (TTL 5 V)

6.5 Encoder (for RA-40 and SE30)

IE3 L with 512 pulses (TTL 5 V)



7 Configuration and structure

Before a configuration is defined, the speeds must first be known.

Limited speed 1 (f_{Speed1}) 1 m/min 0.017 m/s Limited speed 2 (f_{Speed2}) 2 m/min 0.03 m/s

In order to set the speed, the next step is to calculate the maximum frequency generated by the path measuring system while driving.

7.1 Calculation for linear axes

7.1.1 Sensor with 0.01 mm resolution

For this, we first need the resolution of the magnetic sensor (here 0.01 mm with 4x evaluation) $s = 0.00001 \, m * 4 = 0.00004 \, m$

This creates a period length (s) of 0.00004 m.

The formula below can be used to calculate the frequency.

$$f_{Gesch} = \frac{v_{max}}{s}$$
 $f_{Gesch} = \frac{0.017 \frac{m}{s}}{0.00004 m} = 425 Hz$ $f_{Gesch} = \frac{0.03 \frac{m}{s}}{0.00004 m} = 750 Hz$

Since we want to drive at these speeds, we must enter approx. 10 percent more as the tolerance for this speed or frequencies.

$$f_{Gesch} = \frac{v_{max}}{s} + 10\% \qquad f_{Gesch} = \frac{0.017 \frac{m}{s}}{0.00004 m} + 10\% = 467.5 Hz \qquad f_{Gesch} = \frac{0.03 \frac{m}{s}}{0.00004 m} + 10\% = 825 Hz$$

Since the axes also move minimally at 'standstill', a tolerance must also be taken into account here. This was set to 10 increments in the example. In environments that transmit strong vibrations to the handling system, this value must be increased so that a standstill can be signaled correctly.



7.1.2 Sensor with 0.001 mm resolution

For this, we first need the resolution of the magnetic sensor (here 0.001 mm for 4x evaluation) $s = 0.000001 \ m * 4 = 0.000004 \ m$

This creates a period length (s) of 0.000004 m.

The formula below can be used to calculate the frequency.

$$f_{Gesch} = \frac{v_{\text{max}}}{s} \qquad f_{Gesch} = \frac{0}{0.0}$$

$$f_{Gesch} = \frac{0.017 \frac{m}{s}}{0.000004 m} = 4250 Hz$$

$$f_{Gesch 2} = \frac{0.03 \, m/s}{0.000004 \, m} = 7500 \, Hz$$

Since we want to drive at these speeds, we must enter approx. 10 percent more as the tolerance for this speed or frequencies.

$$f_{Gesch} = \frac{v_{max}}{s} + 10\%$$

$$f_{Gesch} = \frac{0.017 \, m/s}{0.000004 \, m} + 10\% = 4675 \, Hz$$

$$f_{Gesch 2} = \frac{0.03 \, \frac{m}{s}}{0.000004 \, m} + 10\% = 8250 \, Hz$$

Since the axes also move minimally at 'standstill', a tolerance must also be taken into account here. This was set to 10 increments in the example. In environments that transmit strong vibrations to the handling system, this value must be increased so that a standstill can be signaled correctly.



7.2 Calculation for rotary axes

For this, we first need the number of increments of the measuring system and the reduction ratio of the gear of the unit.

7.2.1 **SE20** with **50:1** gear

The formula below can be used to calculate the frequency.

$$f_{Gesch 1} = \frac{Ink * i * v_{max}}{360 \circ}$$

$$f_{Gesch 1} = \frac{128 * 50 * 17^{\circ} / s}{360 \circ} = 302,2Hz$$

$$f_{Gesch 2} = \frac{128 * 50 * 30^{\circ} / s}{360 \circ} = 533,3Hz$$

Since we want to drive at these speeds, we must enter approx. 10 percent more as the tolerance for this speed or frequencies.

$$f_{Gesch} = \frac{Ink * i * v_{max}}{360 \circ} + 10\%$$

$$f_{Gesch} = \frac{128 * 50 * 17^{\circ} / s}{360 \circ} + 10\% \approx 335 \, Hz \qquad f_{Gesch} = \frac{128 * 50 * 30^{\circ} / s}{360 \circ} + 10\% \approx 590 \, Hz$$

Since the axes also move minimally at 'standstill', a tolerance must also be taken into account here. This should be set to 34 Hz (approx.10% of reduced speed 1 (fspeed1)). In environments that transmit strong vibrations to the handling system, this value must be increased so that a standstill can be signaled correctly.

7.2.1 **SE20** with **30:1** gear

The formula below can be used to calculate the frequency.

$$f_{Gesch} = \frac{Ink * i * v_{max}}{360 \circ}$$

$$f_{Gesch1} = \frac{128 * 30 * 17^{\circ} / s}{360 \circ} = 181,3Hz \quad f_{Gesch2} = \frac{128 * 30 * 30^{\circ} / s}{360 \circ} = 320 Hz$$

Since we want to drive at these speeds, we must enter approx. 10 percent more than tolerance for this speed or frequencies.

$$f_{Gesch} = \frac{Ink * i * v_{max}}{360 \circ} + 10\%$$

$$f_{Gesch} = \frac{128 * 30 * 17^{\circ} / s}{360 \circ} + 10\% \approx 200 \, Hz \qquad f_{Gesch} = \frac{128 * 30 * 30^{\circ} / s}{360 \circ} + 10\% \approx 350 \, Hz$$

Since the axes also move minimally at 'standstill', a tolerance must also be taken into account here. This should be set to 20Hz (approx.10% of reduced speed 1 (f_{Speed1})). In environments that transmit strong vibrations to the handling system, this value must be increased so that a standstill can be signaled correctly.



7.2.2 RA-40 and SE30 with 50:1 gear

The formula below can be used to calculate the frequency.

$$f_{Gesch} = \frac{Ink * i * v_{max}}{360 \circ}$$

$$f_{Gesch} = \frac{512 * 50 * 17^{\circ} / s}{360 \circ} = 1208 ,88 Hz \qquad f_{Gesch} = \frac{512 * 50 * 30^{\circ} / s}{360 \circ} = 2133 ,33 Hz$$

Since we want to drive at these speeds, we must enter approx. 10 percent more than tolerance for this speed or frequencies.

$$f_{Gesch} = \frac{Ink * i * v_{max}}{360 \circ} + 10\%$$

$$f_{Gesch} = \frac{512 * 50 * 17^{\circ} / s}{360 \circ} + 10\% \approx 1330 \, Hz \quad f_{Gesch} = \frac{512 * 50 * 30^{\circ} / s}{360 \circ} + 10\% \approx 2350 \, Hz$$

Since the axes also move minimally at 'standstill', a tolerance must also be taken into account here. This should be set to 130 Hz (approx.10% of reduced speed 1 (f_{Speed1})). In environments that transmit strong vibrations to the handling system, this value must be increased so that a standstill can be signaled correctly.

7.2.3 RA-40 and SE30 with 30:1 gear

The formula below can be used to calculate the frequency.

$$f_{Gesch} = \frac{Ink * i * v_{max}}{360 \circ}$$

$$f_{Gesch1} = \frac{512 * 30 * 17^{\circ} / s}{360 \circ} = 725,33 Hz \qquad f_{Gesch2} = \frac{512 * 30 * 30^{\circ} / s}{360 \circ} = 1280 Hz$$

Since we want to drive at these speeds, we must enter approx. 10 percent more than tolerance for this speed or frequencies.

$$f_{Gesch} = \frac{Ink * i * v_{max}}{360 \circ} + 10\%$$

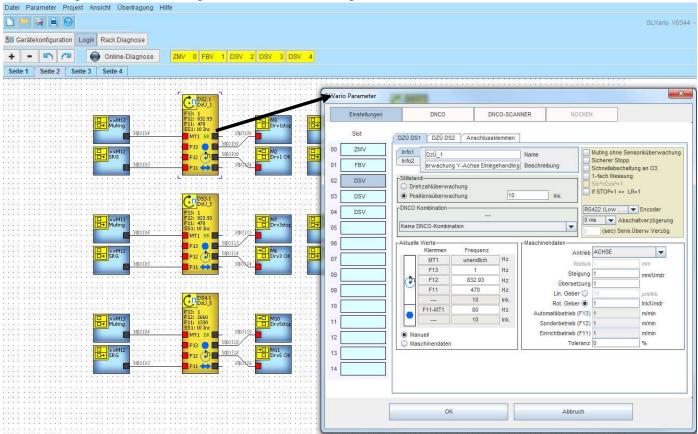
$$f_{Gesch} = \frac{512 * 30 * 17^{\circ} / s}{360 \circ} + 10\% \approx 800 \, Hz \qquad f_{Gesch} = \frac{512 * 30 * 30^{\circ} / s}{360 \circ} + 10\% \approx 1410 \, Hz$$

Since the axes also move minimally at 'standstill', a tolerance must also be taken into account here. This should be set to 80 Hz (approx.10% of reduced speed 1 (fSpeed1)). In environments that transmit strong vibrations to the handling system, this value must be increased so that a standstill can be signaled correctly.



7.3 Settings of SL-VARIO Designer

The settings are made using the SL-VARIO Designer software.



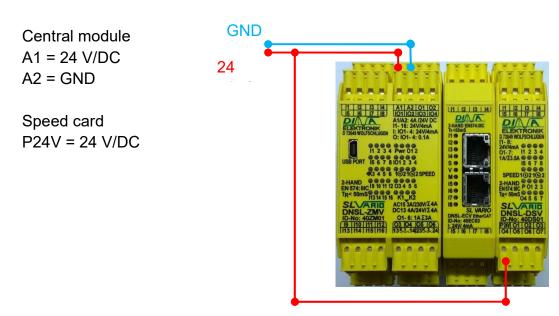
Note: After they are transferred, the frequencies are automatically changed. This comes from the frequency of the integrated quartz crystal.

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Information about wiring

The different cards are connected directly with each other using special plug connectors. These plug connectors are used to realize the power supply of the individual modules and the communication with the central module.

8.1 Power supply of the safety PLC



8.2 Emergency stop circuit

Central module

IO3	Emergency stop, clock	00	IN7	Input 1 for emergency
	output 1	_0 0_		stop
IO4	Emergency stop, clock		IN8	Input 2 for emergency
	output 2			stop

If the contacts are not needed, they can also be bridged directly.

8.3 Safety door circuit

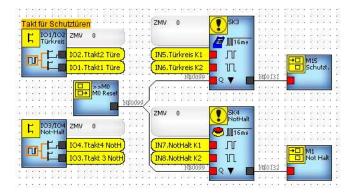
Central module

-00111	Contrain modale											
IO1	Safety door, clock output	0	IN5	Input 1 for safety door								
	1	<u> </u>										
102	Safety door, clock output	·	IN6	Input 2 for safety door								
	2											

If the contacts are not needed, they can also be bridged directly.







8.4 Safe Torque Off (STO)

To ensure safety at reduced speed, it is important that the drive is switched off safely (STO). Therefore, it is important to use a double contact as shown in the connection diagram. The connection diagrams show 2 variants of how to wire the STO circuit.

8.4.1 STO triggering for axes (Variant 1)

To trigger the STO for all axes simultaneously as soon as a safety violation occurs, the following connection diagram must be used.

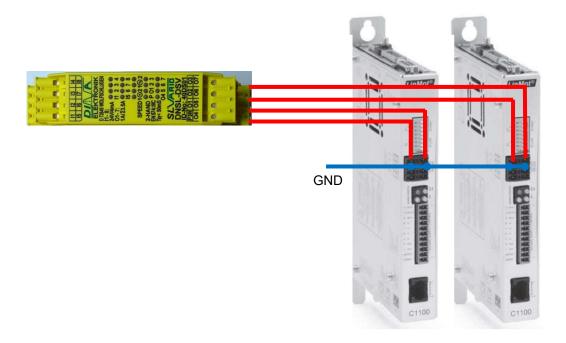
Central modu	le	Servo co	ontr	oller			
Q13 24 V							
Q14 X33.8		X33.8	Q1	14			
Q23 24 V							
Q24 X33.4		X33.4	Q2	24			
		X33.7	G	ND	000		000
		X33.3	G	ND			O.L
					1	ALIA.	The same
	A.A.					LinMot	LinMot
	1 12 15 16	13 14 A1 A2 O1 O2 17 18 IO11IO21IO3 IO	31			2- 600	
	ELEKTRO D 72849 WOLF	II- 16: 24V/4mA I: IO1- 4: 24V/4m/ O: IO1- 4: 0.1A			-		128
	USB PORT	11 2 3 4 Pwr 012 15 6 7 8 101 2 3 4 K3 4 5 6 1021 G 2 SPEED	Ш	GN	ID ID		The second
	2-HAND EN 574:IIIC	0K3 4 5 6 1⊙21G;2SPEED ○○○○ ○○○○ 19 10 11 12 03 4 5 6	Ш	Ű,		8	65
	SL\/F DNSL- ID-No: 40	19 10 11 12 03 4 5 6 13 14 15 16 K1 _ K2 RID				· · · · · · · · · · · · · · · · · · ·	10E 10E 10E 10E
	13 14	03 04 05 06 06 15 116 1353-14 235-3-2	4				が成
		· I · · ·			*		
	24					C1100	C1100

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8.4.2 STO triggering for a single axis (Variant 2)

The following connection diagram can be used to trigger the STO for individual axes as soon as a safety violation of the respective axis occurs.

Spe	ed module	Servo controller 1			Servo controller 2		
Q4	X33.8(1)	X33.8	Q4				
Q5	X33.4(1)	X33.4	Q5				
Q6	X33.8(2)				X33.8	Q6	
Q7	X33.4(2)				X33.4	Q7	
		X33.7	GND				
		X33.3	GND				

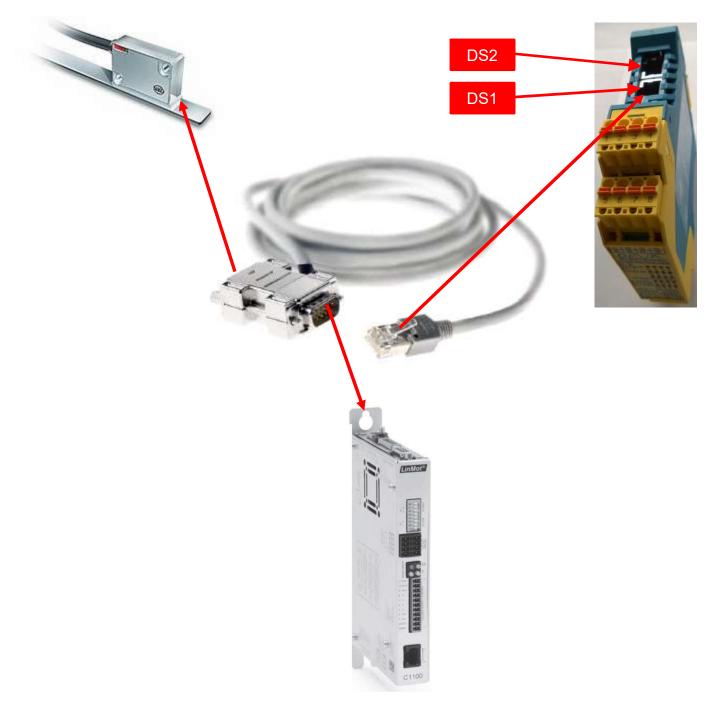




8.5 Path measuring system

For the path measuring system, it is recommended to use the standard cable adapters. They split the signal lines of the path measuring system so that the signals are applied to both the servo controller and the safety PLC.

The cable adapter has 3 connections (Sub-D plug, 15-pin / Sub-D socket, 15-pin / RJ45 plug). It is connected directly to the servo controller with the Sub-D connector, to X13 of the servo controller. The magnetic sensor is plugged into the Sub-D socket. The RJ45 connector is connected to DS1 or DS2 of the respective speed card.



Connection diagram



9 Operation

9.1 Selecting the operating mode

In our example, three operating modes are used: Reduced speed 1, reduced speed 2, and automatic mode (no monitoring of the speed).

The IN1, IN2 and IN3 inputs are available on the central module to select the respective operating modes. The inputs are activated by the 24 V connection.

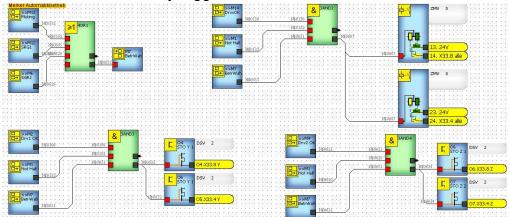
The table below shows how to select which operating mode.

Inpu	ıts		Operating mode
IN1	IN2	IN3	
Х			SLS 1
X		Х	SLS 2
Х			Automatic mode
(24)	Visa	alway	s applied to X)



9.2 Switching between the operating modes

To achieve a safe operating state, the SLS must be selected with the safety door open. Otherwise, the STO is automatically triggered at the servo controller and the axis is therefore de-energized.



If required, the changeover from automatic to SLS can be delayed via the timers.

It must be noted that the SLS is only active after the times ZW3/ZW1 have elapsed.

This may give rise to potential problems:

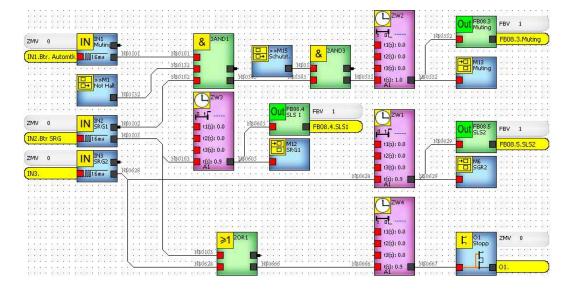
Times too long: Safe operation cannot be guaranteed

Times too short: Axles cannot be braked fast enough to the safe speed → Violation of the SLS

→ STO → Axles are de-energized.

The time ZW2 should always be set approx. 10% higher than ZW1/3/4.





9.2.1 Important information

- 1. In automatic mode, the emergency stop circuit and the safety door circuit must be closed
- 2. In SLS mode, the emergency stop circuit must be closed
- 3. If an enabling switch is used, it must also be actuated when switching to SLS operation. If this is not actuated, this automatically leads to an STO.
- 4. Braking can be implemented using a corresponding run command via the PLC. For example, an absolute run command can be sent with the same target position and limited speed, acceleration and deceleration.

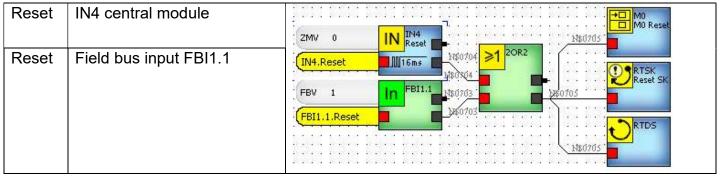
Alternatively, the /Abort function (control word) can be used. This function is then assigned to a digital input of the servo controller. This function completely decelerates the axle, but then the control remains active.

The /Quickstop should <u>not</u> be used, as it automatically leads to an STO.

Note: The digital inputs on the controller are not safe inputs!

9.3 Resetting the safety PLC

If an error has occurred, e.g. due to exceeding the speed, the safety PLC requires a reset. This can be carried out either via the IN4 input on the central module or via the field bus (FBI1.1). If you do not want to carry out a reset, but want the safety PLC to carry it out automatically, you can set the IN4 input to 24 V. However, no errors are output during an automatic reset.





9.4 Display of the operating state

Digital outputs

Cen	tral module	LARA LARA	Axis mo	15551	
Q1	Stop for changeover from		Q1	Standstill, axis 1	2222
	automatic to SLS (Abort)	1			11 12 13 14 15 16 17 18
Q2	Standstill	ELEKTRONIK D72849 WOLFSCHLUGEN O: IO1-4: 24V/4mA O: IO1-4: 0.1A	Q4/5	Axis 1 OK	ELEKTRONIK D72549 WOLFSCHLIGEN 11-8:
Q3	Error	11 2 3 4 Pwr 01 2 USB PORT 15 6 7 8 101 2 3 4	Q2	Standstill, axis 2	01-7: 11 2 3 4 1A/23.5A 0 0 0 15 6 7 8
		43 4 5 6 1021G2SPEED 2-HAND EN 574:IIIC 19 10 11 12 03 4 5 6	Q6/7	Axis 2 OK	SPEED1@21@2 2-HAND
		TR< 50mS 131415 16 K1 K2 SL\ARID AC15 3A/230V/Σ4A DNSI ZMV DC13 4A/24V/Σ4A	Attentio	on!	TR<50mS 04 5 6 7
		ID-No: 40ZM01 O1-6: 1Α Σ3Α	If you us	se the " STO triggering for a	DNSL-DSV ID-No: 40DS01 P3M 01 02 03 04 05 06 07
			single a	xis " variant, the input of	0000
			your PL	C must be protected	
			against	inductive loads.	Car Class

10 Field bus assignment - input/output

10.1 *Input bytes*

FBI1.1	Reset
FBI1.2	Free
FBI1.3	Free
FBI1.4	Free
FBI1.5	Free
FBI1.6	Free
FBI1.7	Free
FBI1.8	Free



All other input bytes are not occupied.

10.2 Output bytes

FBO1.1	Error, axis 1	FBO2.1	Error axis 9	
FBO1.2	Error, axis 2	FBO2.2	Error, axis 10	
FBO1.3	Error, axis 3	FBO2.3	Error, axis 11	
FBO1.4	Error, axis 4	FBO2.4	Error, axis 12	
FBO1.5	Error, axis 5	FBO2.5	Error, axis 13	
FBO1.6	Error, axis 6	FBO2.6	Error, axis 14	
FBO1.7	Error, axis 7	FBO2.7	Error, axis 15	
FBO1.8	Error, axis 8	FBO2.8	Error, axis 16	
FBO3.1	Error, axis 17	FBO4.1	Standstill, axis 1	
FBO3.2	Error, axis 18	FBO4.2	Standstill, axis 2	
FBO3.3	Error, axis 19	FBO4.3	Standstill, axis 3	
FBO3.4	Error, axis 20	FBO4.4	Standstill, axis 4	
FBO3.5	Error, axis 21	FBO4.5	Standstill, axis 5	
FBO3.6	Error, axis 22	FBO4.6	Standstill, axis 6	
FBO3.7	Error, axis 23	FBO4.7	Standstill, axis 7	
FBO3.8	Error, axis 24	FBO4.8	Standstill, axis 8	
FBO5.1	Standstill, axis 9	FBO6.1	Standstill, axis 17	
FBO5.2	Standstill, axis 10	FBO6.2	Standstill, axis 18	
FBO5.3	Standstill, axis 11	FBO6.3	Standstill, axis 19	
FBO5.4	Standstill, axis 12	FBO6.4	Standstill, axis 20	
FBO5.5	Standstill, axis 13	FBO6.5	Standstill, axis 21	
FBO5.6	Standstill, axis 14	FBO6.6	Standstill, axis 22	
FBO5.7	Standstill, axis 15	FBO6.7	Standstill, axis 23	
FBO5.8	Standstill, axis 16	FBO6.8	Standstill, axis 24	
	_			
FBO7.1	Free	FBO8.1	Error	
FBO7.2	Free	FBO8.2	Standstill of all axes	
FBO7.3	Free	FBO8.3	Muting input status	
FBO7.4	Free	FBO8.4	Limited speed 1 input status	
FBO7.5	Free	FBO8.5	Limited speed 2 input status	
FBO7.6	Free	FBO8.6	Free	
FBO7.7	Free	FBO8.7	Free	
FBO7.8	Free	FBO8.8	System OK	



11 SL-VARIO Designer software

The safety PLC is programmed with the SL-VARIO Designer software – V0344 that is supplied free of charge.

This description is only intended as a rough guide. A detailed description can be found on the CD supplied by the manufacturer and on the flash drive in the central module.

Note:

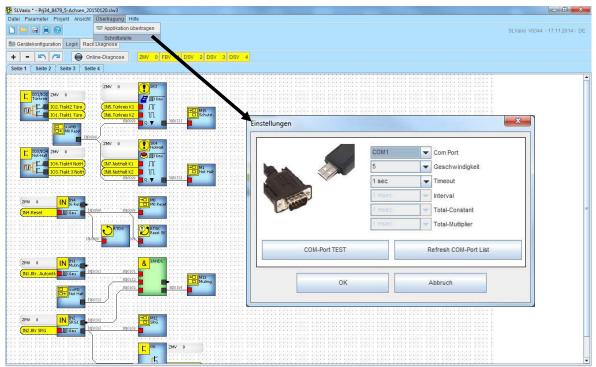
In order to perform an online diagnosis of the program, the version stored on the PC must be identical to that on the safety PLC.

11.1 System prerequisites

- Operating system: Windows XP, Windows Vista, Windows 7, Windows 8 (only after consultation with DINA)
- Main memory: min. 512 MB
- JAVA Runtime Environment (JRE): Min. version 6, Update 16
- USB port
- Connecting cable: To establish a connection to the central module, a conventional USB cable (A plug to B mini plug) is required. This is connected to the mini USB socket labeled 'USB PORT'.

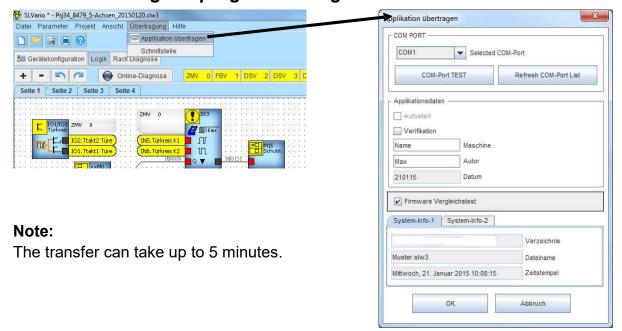


11.2 Setting the interface

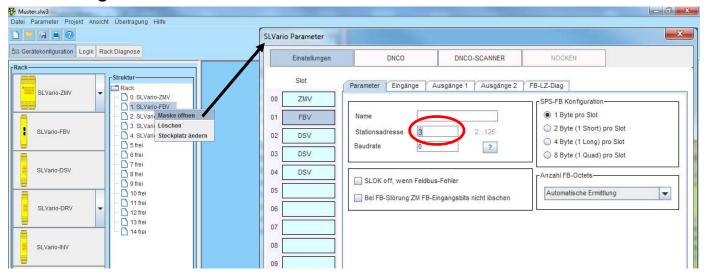




11.3 Transferring the program/settings



11.4 Setting the field bus address



12 Please note

Depending on the mode, motor used and wiring, there can be different response times. The safety module requires approx. 11 ms from detection of the excessive speed to the falling edge at the output with '1x measurement' and active rapid switch-off directly in the speed monitoring module (semiconductor output Q3). If the relay contact on the central module is used, this time increases accordingly.

The time until the STO relay on the controller itself drops out must also be taken into account in the customer's safety consideration, and is between 3 ms and 20 ms depending on the external wiring.

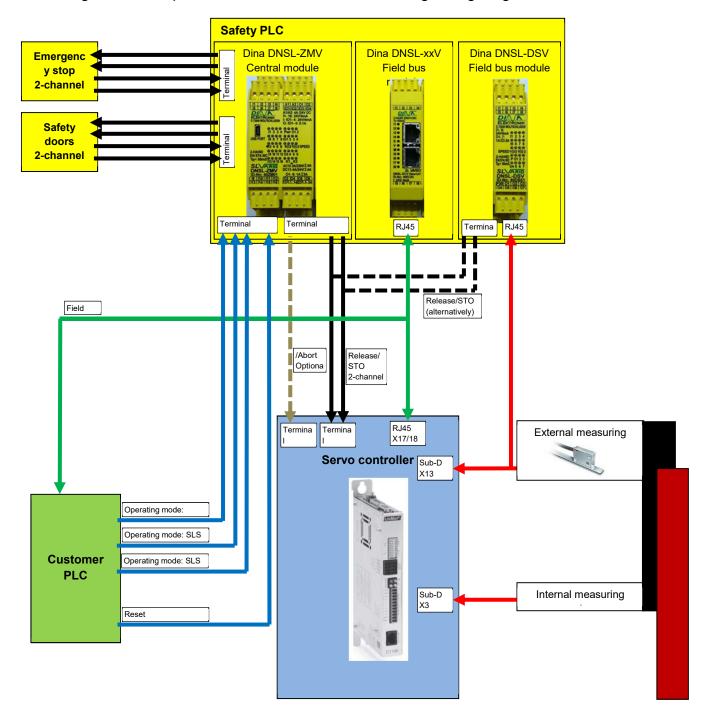


13 Achievable performance level

The redundant design and monitoring of all safety-relevant components and the speed monitoring on the safety PLC ensure one-fault safety.

This enables required performance level 'd' to be achieved.

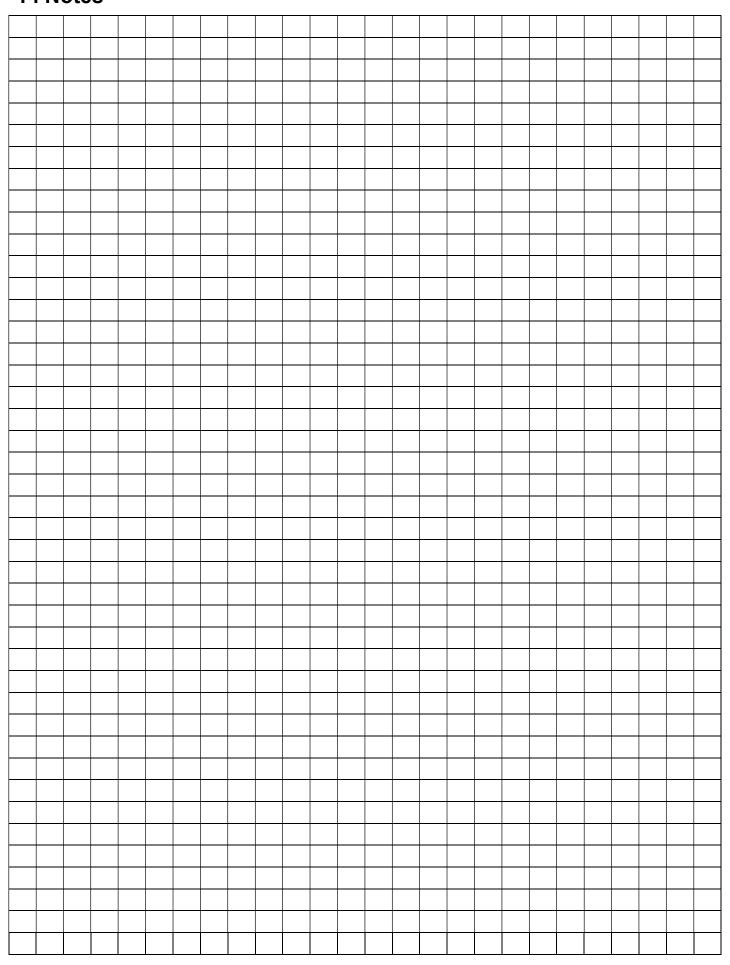
The wiring must be implemented as shown in the following wiring diagram.



22

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14 Notes



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15 Support

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